

# Graphite packing rings

By ESA member Jan Kasprzyk

Die-formed expanded graphite rings are widely used as gland packings in modern process valves for higher temperatures. The development of this sealing solution started in the 1970s and is defined by the characteristics of the expanded graphite material.

The distinctive material features of expanded graphite rings include:

- Low friction coefficient, estimated at a level of 0.1 for wet friction and 0.16 for dry friction
- Remarkable chemical resistance against most process fluids, including all fluids used in energy generation
- High resistance to nuclear radiation making them eminently suitable for applications in nuclear engineering
- Resistance to high temperatures exceeding the resistance of the most common sealing materials
- Relatively low cost
- High resistance to compression
- On the negative side, low resistance to tensile and shear forces

It is also significant that in terms of the applications where gland packings are used, our knowledge of this material and our experience is the most extensive. Initially in the seventies, the rings were made directly from expanded graphite particles by filling them into a tool or even by forming directly in the device (pump or valve). In this case, a problem occurred related to the low density of the expanded graphite particles and the high compression set. Because of this graphite foils with a higher density of 0.7 - 1 g/cm<sup>3</sup> were used to form rings because they are easier to handle.

# **Graphite foil**

Graphite foil is thus currently the basic intermediate product used in the production of graphite gland packings and graphite seals in general.

Such foil is supplied by manufacturers of graphite products in different densities (usually 0.7-1.0 g/cm<sup>3</sup>), carbon contents (in process seals carbon contents of 95-99.9% of carbon are applied), in different thicknesses (0.3-1.0 mm) and with various modifying additives.

Graphite foil materials can also differ in terms of the content of soluble chlorides, fluorides and sulphur, which have an impact on the development of corrosion, and in the amount of traces of rare earth metals which have an impact on the rate of oxidation. These properties are not always specified by the supplier.

While the thickness of the foil or its density may be treated as a purely technological quality, the remaining material characteristics have a fundamental impact on the functionality, durability and operational reliability of a packing.

### **Purity and modifications**

Thus, high purity (the higher the carbon content, the higher is the purity) influences the sealing efficiency or tightness, the corrosive behaviour and the rate of oxidation. In Europe, two graphite purities are used in process applications: the so-called industrial grade, exhibiting a carbon content of at least 98% (this type of graphite is most often used in the production of seals) and the so-called nuclear grade used in nuclear engineering and exceptionally important devices such as critical fittings and valves or those in severe operating conditions.

The content of chlorides, fluorides and sulphur has a great impact on the rate of corrosion – particularly in steam and water environments. The content of these impurities is limited to 50 ppm in case of chlorides for the industrial grade foil and 20 ppm in case of the nuclear grade. This is in line with the DIN 28090 standard. The content of sulphur is not always specified but in case of good quality graphite, it is below 500 ppm, preferably 300 ppm. The content of elements such as sodium (Na), potassium (K), manganese (Mn) and magnesium (Mg) has a great impact on the durability of graphite at elevated temperatures (see Valve World - September 2016). Thus, especially in applications at over 350 °C, the graphite quality should be carefully selected.

Irrespective of the selection of the base material, one of the methods to increase the resistance to oxidation is to add oxidation inhibitors to the graphite foil. This technology has been mastered and, along with other structural procedures, it allows the use of graphite seals in temperatures of fluids exceeding 600 °C. Other graphite modifications include the introduction of a corrosion inhibitor which prevents or delays the development of



Figure 1: A folded structure in a pure graphite ring and in a metal foil reinforced graphite ring.



Figure 2: Three forms of rings: Endless, with a single cut and with two cuts.

## COLUMN





Figure 3: Cross-section with a turned jacket.

corrosion that is especially high in raw water. Another graphite modification is coating it with a thin layer of PTFE, which decreases the stem-packing friction coefficient whilst increasing the tightness.

#### **Graphite rings**

Apart from the various graphite foil qualities, the gland seals made from them are also distinctive in terms of varying structural forms and density. The density of the graphite rings as supplied is normally in the range from 1.3 to 1.8 g/cm<sup>3</sup>. Rings with a density of 1.8 g/cm<sup>3</sup> can be used even in pressures exceeding 300 bar.

This density is a structural characteristic of the rings and with higher densities the pressure resistance is increased and higher contact pressures can be achieved. In terms of the structural forms of graphite rings, one may distinguish structures intended for valve stems or for static applications in self-sealing covers of fittings and valves and other static joints. In such cases the graphite rings can also contain metal components.

As mentioned earlier, graphite rings are made by means of die-forming graphite tape which is wound into a tool. As a result of this process, the lamellae inside the ring are arranged in a characteristic folded shape (Figure 1), which results in the fact that the axially applied pressure is efficiently converted into radial pressures with a pressure conversion coefficient (K) for these rings amounting to approximately 0.9. Seals for valves stems, when they do not contain metal components, may have an endless form, or a single or double cut diagonal to the ring's axis (Figure 2). The cuts facilitate the installation of the ring during operation maintenance services, as they do not require the removal of the valve drive.

Expanded graphite, as mentioned at the beginning of this article, is characterized by very low breaking strength. In practice, this means that when axially compressed it may be extruded into the gaps between the gland and the stem, the gap at the bottom of the stuffing box and the gap between the gland and the wall of the stuffing box. As a result of this in high pressure applications and in the case of large diameters, where the gaps into which the graphite may be introduced are wider, special structural procedures are applied to minimize the extrusion. One method used is to produce graphite rings that are laterally reinforced with metal foils – they constitute a type of laminate with flat, alternately arranged layers of graphite and metal foil. In this case, however, the transmission of axial stress into radial stress is only slight and such rings are therefore categorised as "antiextrusion rings" and not "sealing rings". Another method of reinforcement consists in die forming a metal-graphite laminate reeled on a mandrel. In this case, a form of two-component fold is formed in the crosssection of the ring (Figure 1). Its properties are also far from the basic structure's properties. Here the rings are usually used as anti-extrusion rings as well, while they may perform a sealing function in case of high pressures. These rings are also used as spacer rings when filling the bottom space in long stuffing boxes. It is assumed that the maximum number of rings in a stuffing box is 6 – this results from the axial distribution of the contact pressures. In static applications and sometimes in quasi-static applications, graphite rings used for high-pressure operation combined with large clearances (usually related to large diameters or high wear of the fittings and valves) are produced with steel jackets at the corners (Figure 3). Such a jacket closes the gap and prevents

the extrusion of the graphite. The jackets

Figure 4: Cross-section of a complex set of 2 trapezoid rings and adapter rings.

may be of various thicknesses between 0.5 and 1.5 mm and be made of different materials such as austenitic steel or nickel alloy. Such rings are most frequently used in self-sealing covers and medium and high-pressure fittings and valves. In this case, the cross-section of the ring may be square, rectangular or trapezoidal. A variety of other reinforcement methods are used such as the incorporation of a metal mesh, springs in the ring corners and geometrically complex combinations of follower rings and steel o-rings. By combining different shapes, crosssections and/or densities of rings it may be possible to optimize the set in terms of its sealing integrity, lower the friction on the valve stem, minimize the wear or decrease the contact pressures. Some specific graphite set designs using these techniques are patented by sealing manufacturers.

The author is grateful to Jacek Faruga for provision of the figures.

has produced this article as a guide sealing systems and devices. These articles are published on a regular basis, as part of their commitment to users, contractors and OEM's, to help to find the best solutions for sealing challenges and to achieve maximum, safe performance during the lifetime of the seal. The ESA is the voice of the fluid sealing industry in Europe, collaborating closely with the Fluid Sealing Association (FSA) of the USA. Together, they form the key global source of technical knowledge and guidance on sealing technology, which is the basis for these articles. For more information, please visit www.europeansealing.com